

# Thermoelectric conversion in tandem thermoelectric-photovoltaic applications

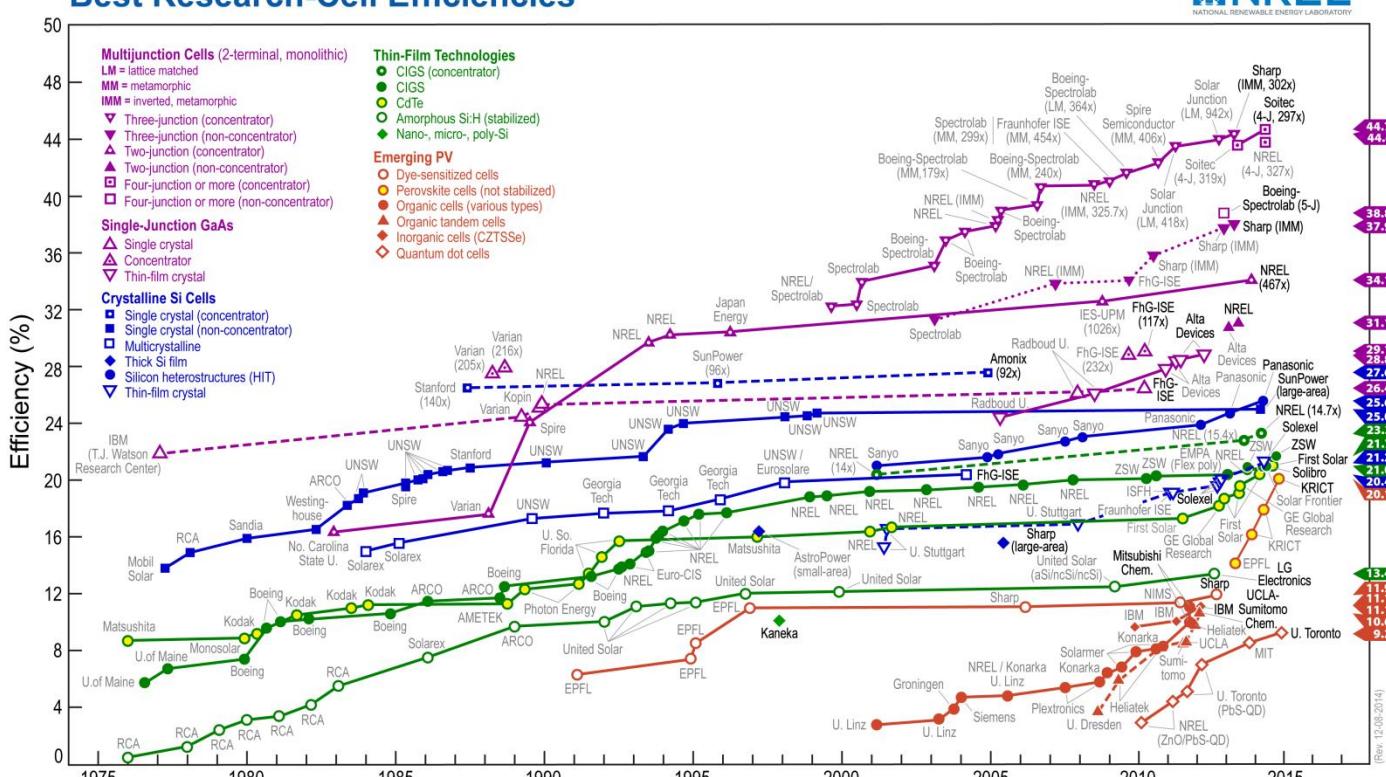
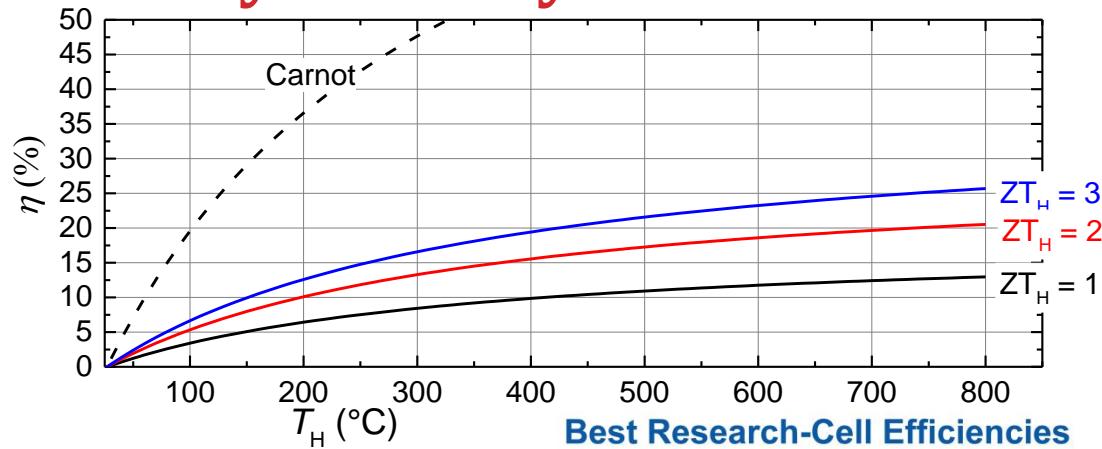
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# Outline

- A short history of TE solar converters:
  - Pure solar thermoelectric generators (STEGs)
  - Hybrid co-generative STEGs (HCG-STEGs)
  - Hybrid thermoelectric-photovoltaic generators (HTEPVGs)
- Why (and when) we may need STEGs
- HTEPVs: working out the power balance in a single-junction device
  - The  $T$ -dependent Shockley-Queisser limit
  - HTEPVGs recovering PV hot carrier energy
  - HTEPVGs also recovering low-energy photons
  - Shaping the TEGs
- Opportunities and challenges:
  - PV old goodies redux
  - TEG geometry and TE materials
- Some conclusions

# Why we may need TEs for solar conversion

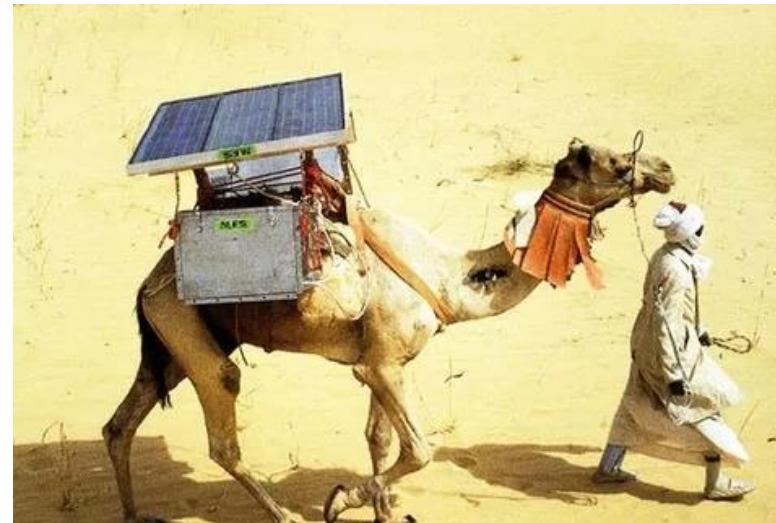


# Why we may need TEs for solar conversion

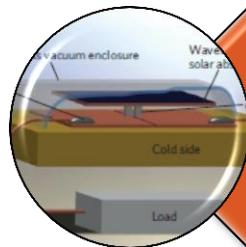
- TE efficiency lags far behind PVs
- It is unrealistic to expect short-term dramatic improvements of TE figures of merit

However:

- TEs allows for thermal concentration, a space-saver
- TEs may operate in harsh environments



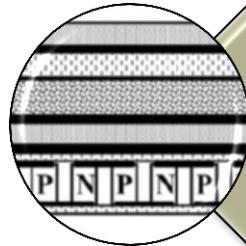
# How TEGs may help



STEG: full thermal conversion



HCG-STEG: TEGs + thermal cogeneration

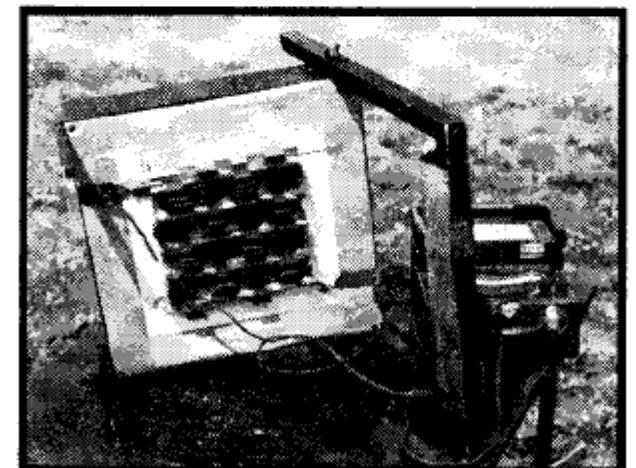
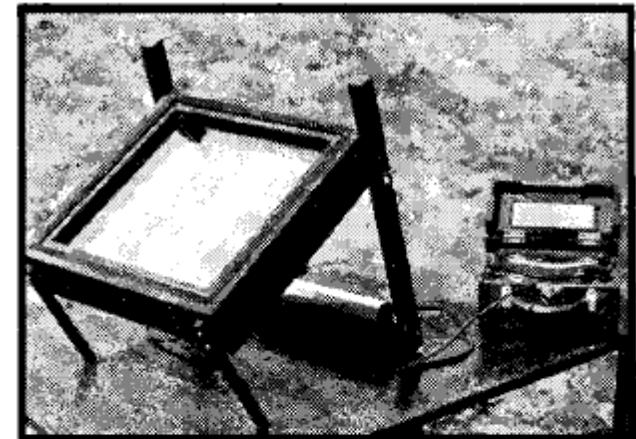
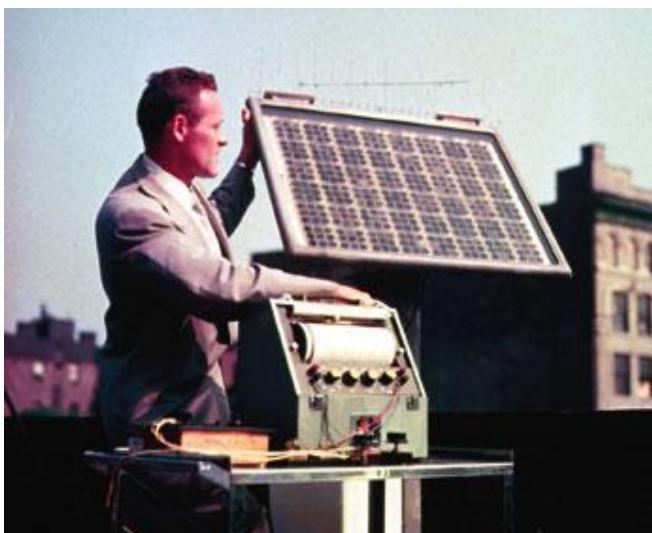


HTEPV: two-stage  
PV + TEGs

# STEGs: Pure solar TEGs

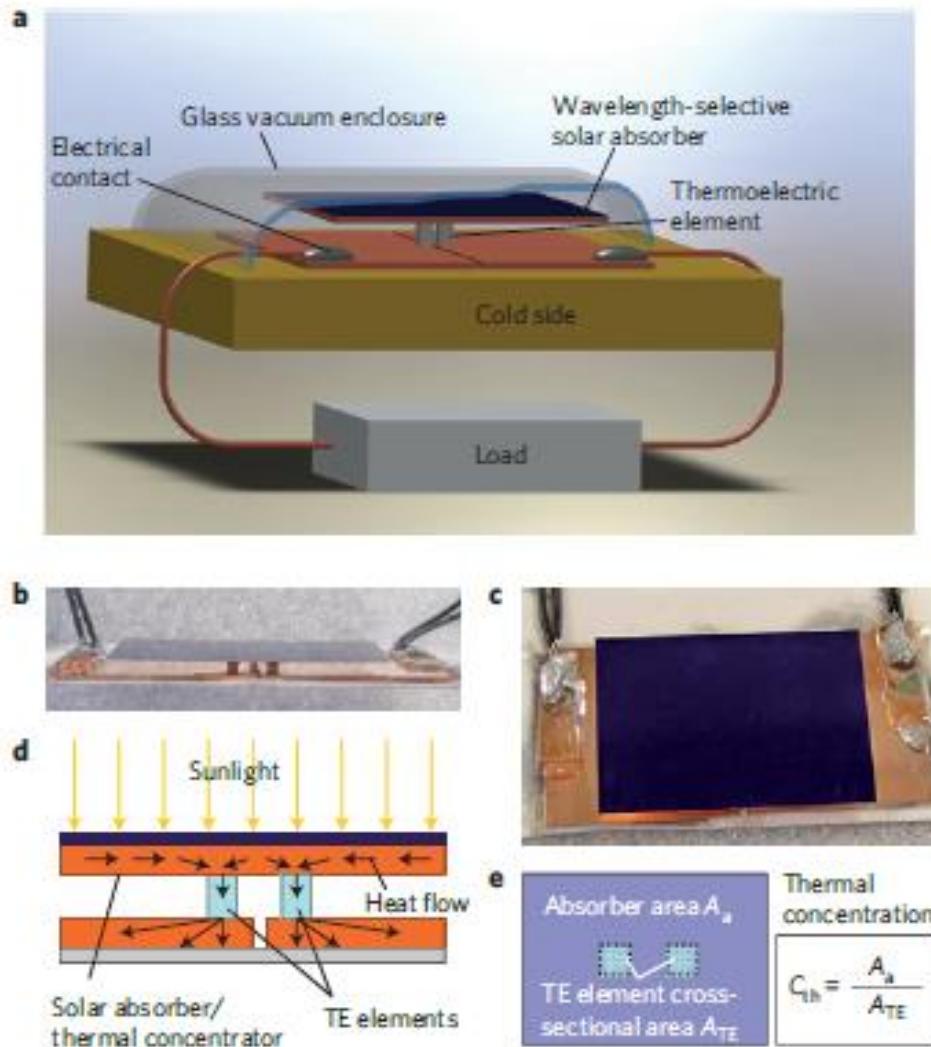
M. Telkes, J. Appl. Phys., 25 (1954) 765

- Convert solar energy into heat and then into electric energy by TEGs
- Operate with  $T_H = 300 - 1000 \text{ }^\circ\text{C}$  using from PbTe/PbSe to SiGe alloys
- Telkes' prototype based upon ZnSb and  $\text{Bi}_{0.91}\text{Sb}_{0.09}$  ( $ZT=0.4$ )
- $\eta = 0.63 \% @ 70\text{ }^\circ\text{C}; \eta = 3.35 \% @ 247\text{ }^\circ\text{C}$



Bell labs, 1954 – efficiency of 4%

# STEGs: Pure solar TEGs



*Non-optically concentrated*  
 STEGs now reach  $\Delta T = 100$  K  
 with  $\eta = 4.6\%$  using ns- $\text{Bi}_2\text{Te}_3$

- thermal concentrators
- quasi-ideal thermal insulation
- selective solar absorber (absorptivity  $\approx 0.95$ , emissivity  $\approx 0.2$ )

Cost  $\approx 0.17$  \$/W (compared to  
 1.6 \$/W for optically  
 concentrated)

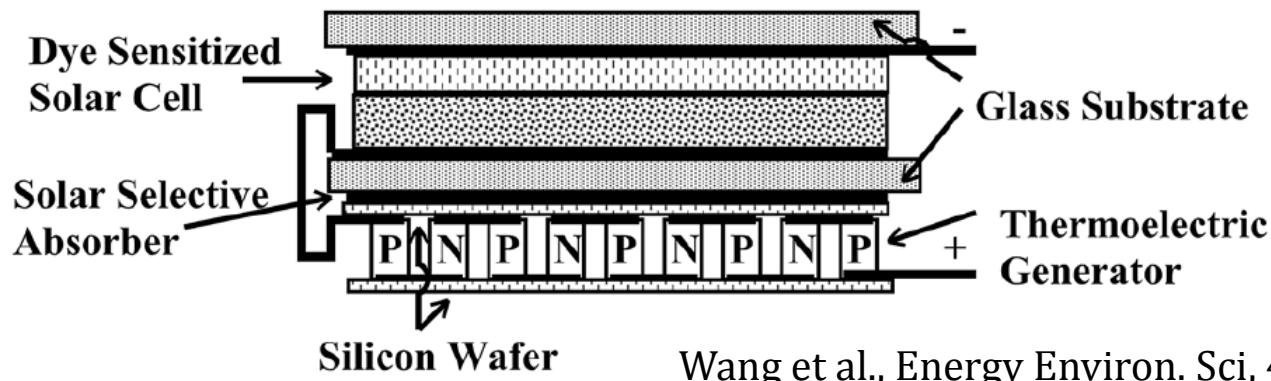
# Hybrid co-generative TEGs

- STEGs using output heat flow to heat water or likely
- Electrical efficiency of <5 %
- Typical plant may cogenerate  $0.12 \text{ kW}_e \text{h} + 1.2 \text{ kW}_{\text{th}} \text{h}$



# Hybrid TE-PV (HTEPV) generators

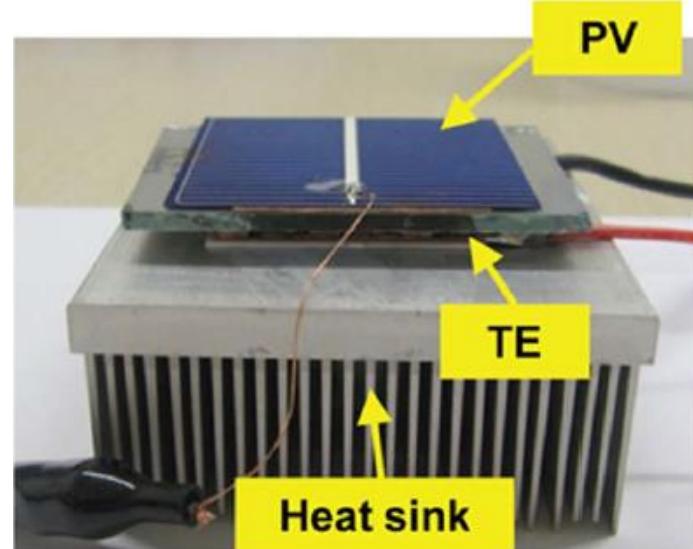
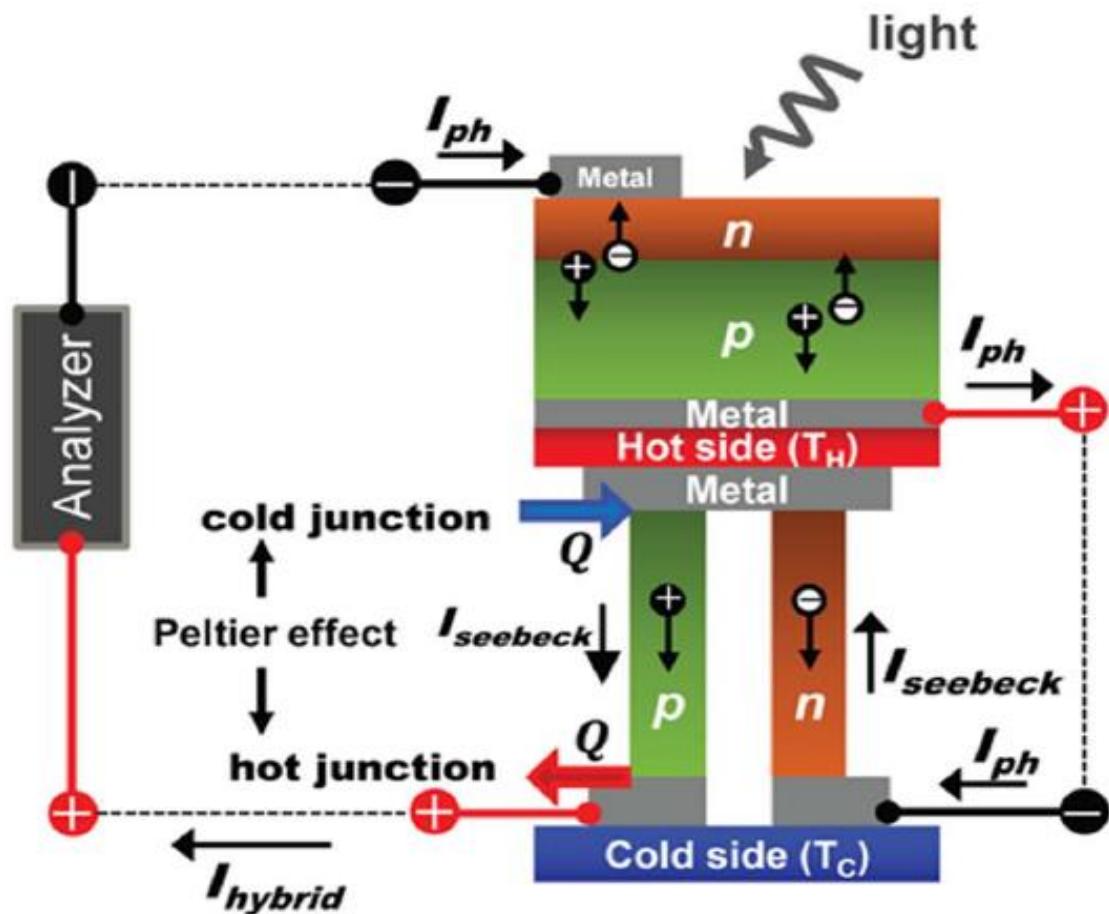
- TEG reuses the heat released by the PV
- Possibly optically concentrated



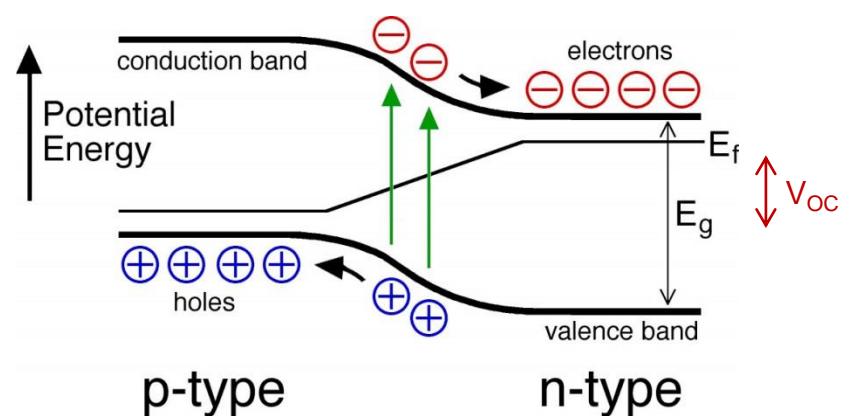
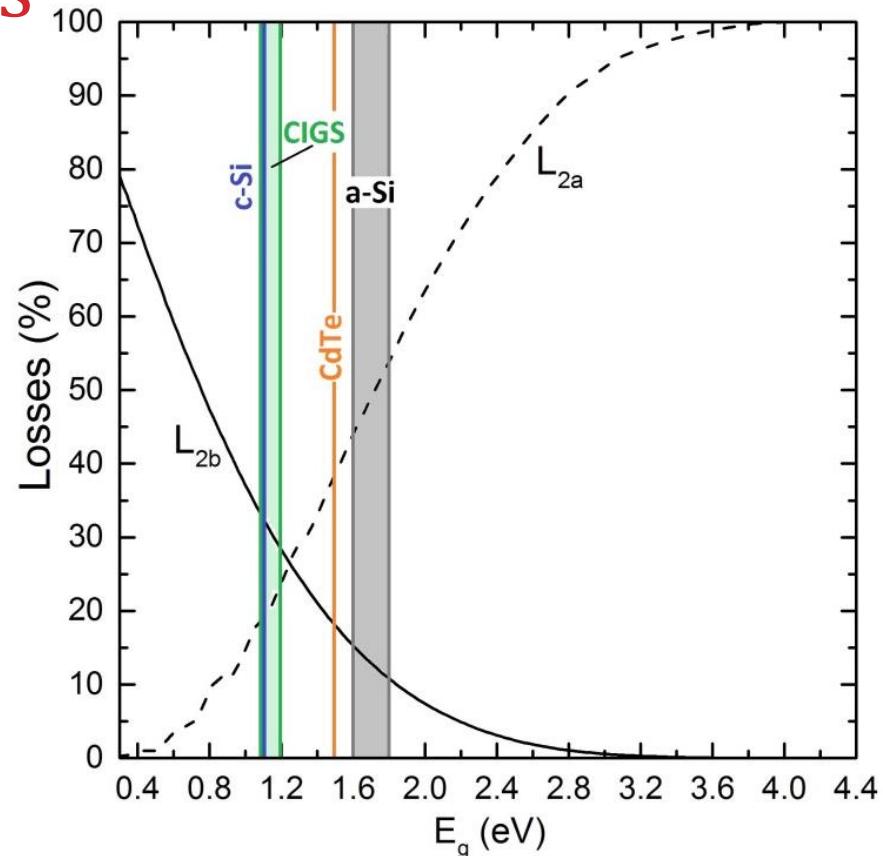
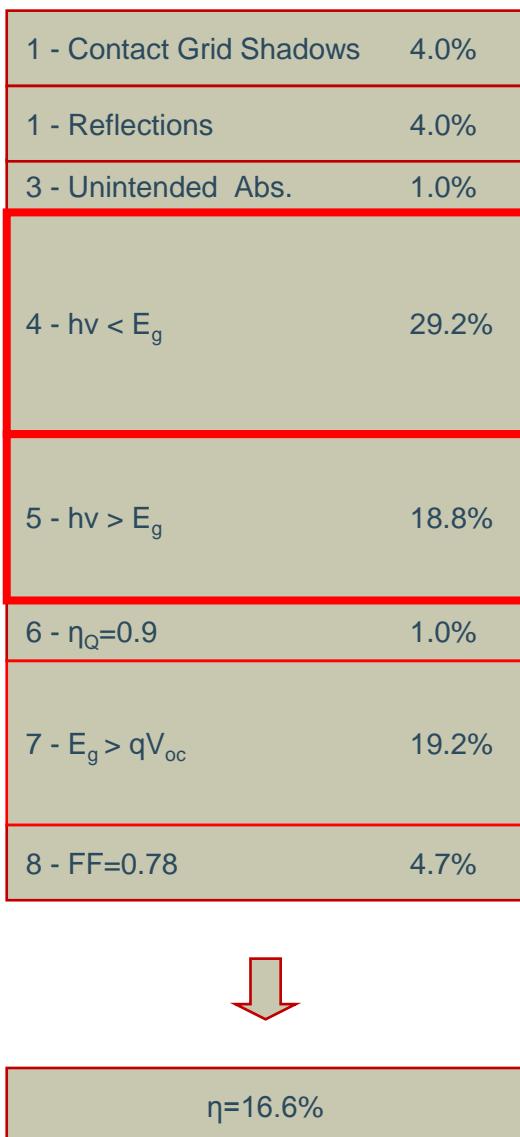
Wang et al., Energy Environ. Sci, 4 (2011) 3676

- DSSC + SSA + TEG( $\text{Bi}_2\text{Te}_3$ ) achieve  $\eta_{\text{tot}} = 13.8\%$ ,  $12.8 \text{ mW/cm}^2$

# The basic principles of HTEPV design



# SJ solar cell model: Losses



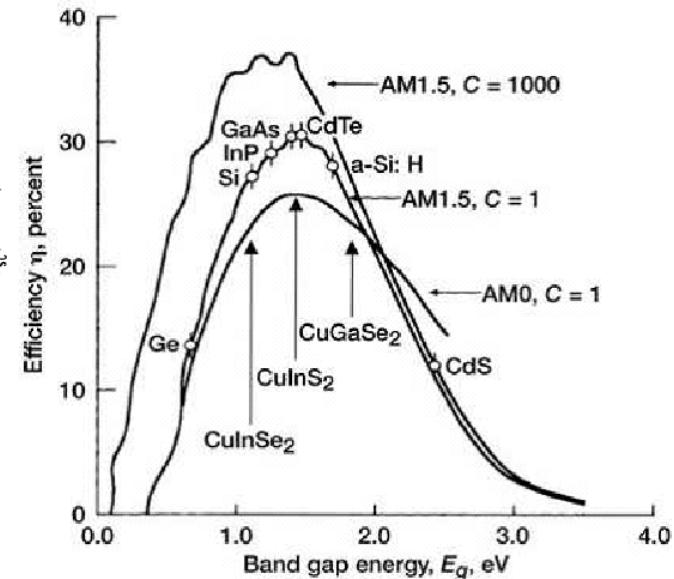
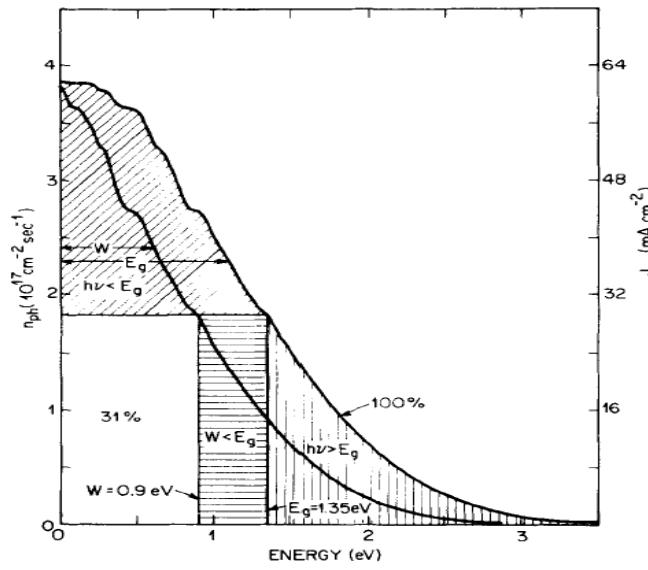
# SJ solar cell model: the SQ limit

Thermodynamic Limit

$\approx 95\%$

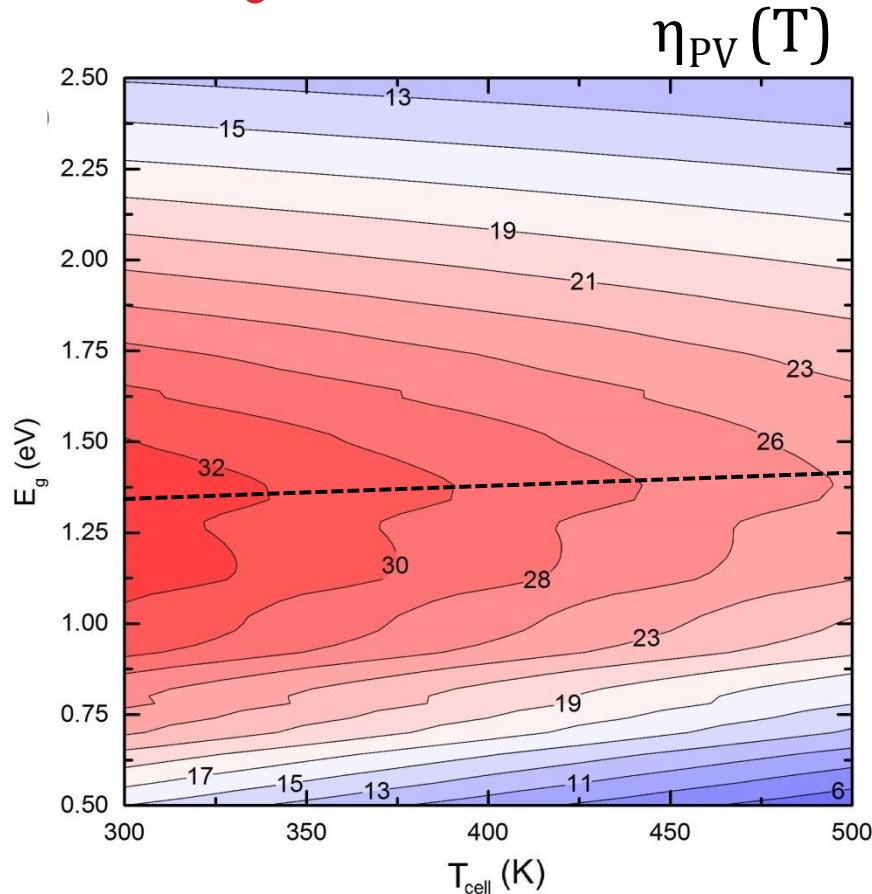
Shockley & Queisser  
Limit  $\approx 31\%$

at  $E_g \approx 1.35$  eV

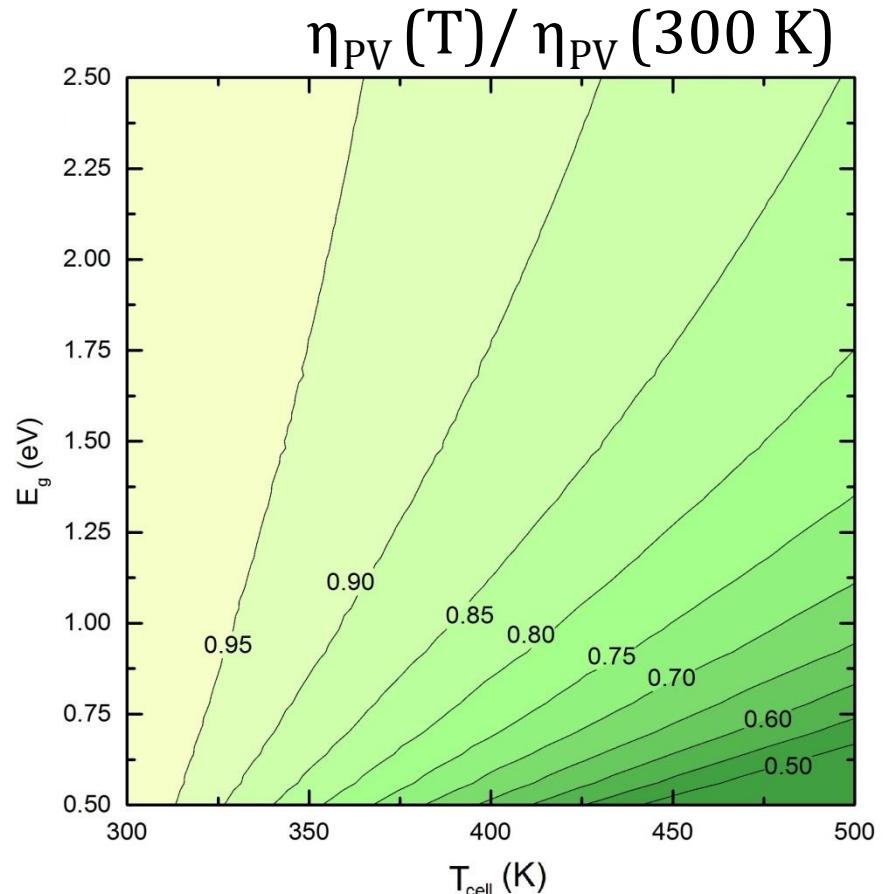


- i. all photons with  $E_\gamma > E_g$  are absorbed, while photons with  $E_\gamma < E_g$  produce no effect
- ii. unitary quantum efficiency
- iii.  $T_{\text{cell}} = T_a$
- iv. the only mechanism of electron-hole recombination is radiative

# The SQ radiative limit

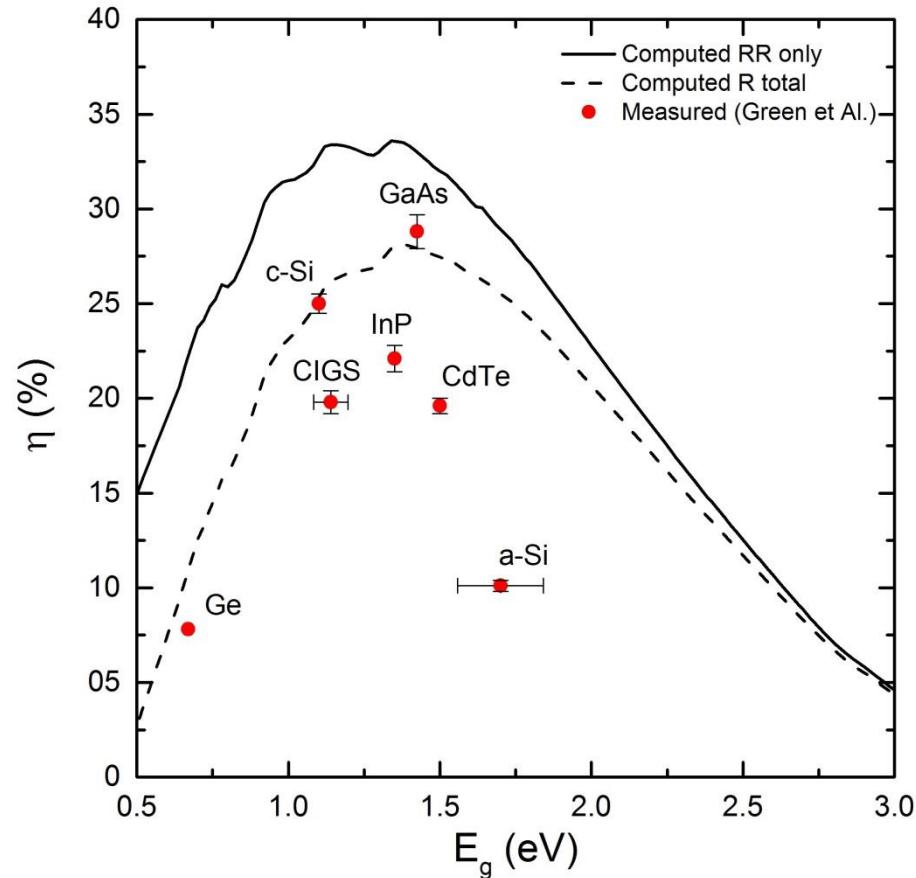
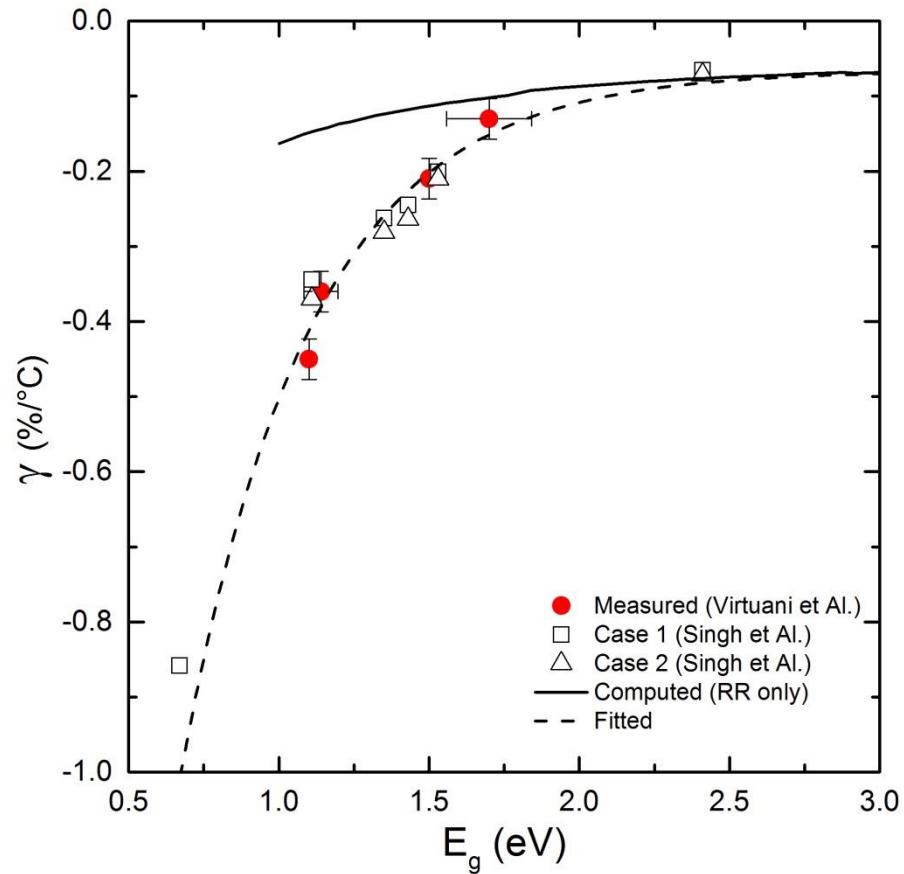


$\max \eta_{PV} (300 \text{ K}) = 33.6 \text{ \%}$  at 1.36 eV



$E_g$  effect on  $\eta_{PV}$  decreases

# Accounting also for recombination

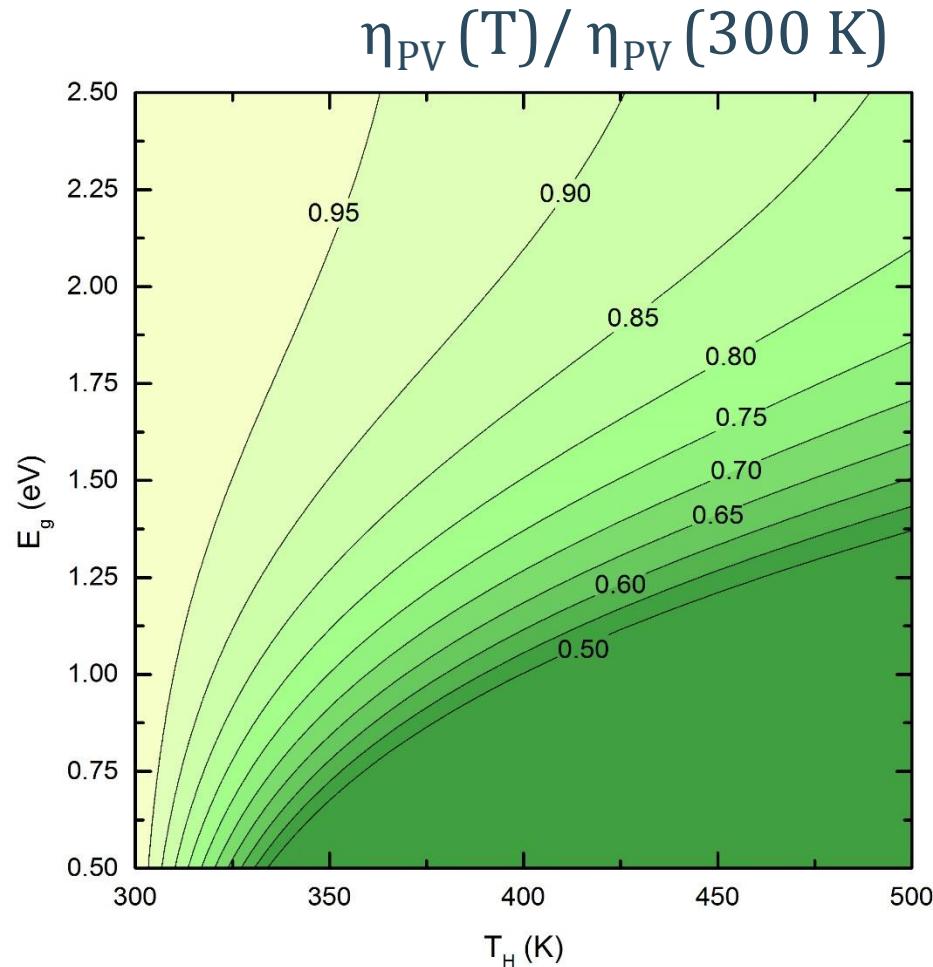
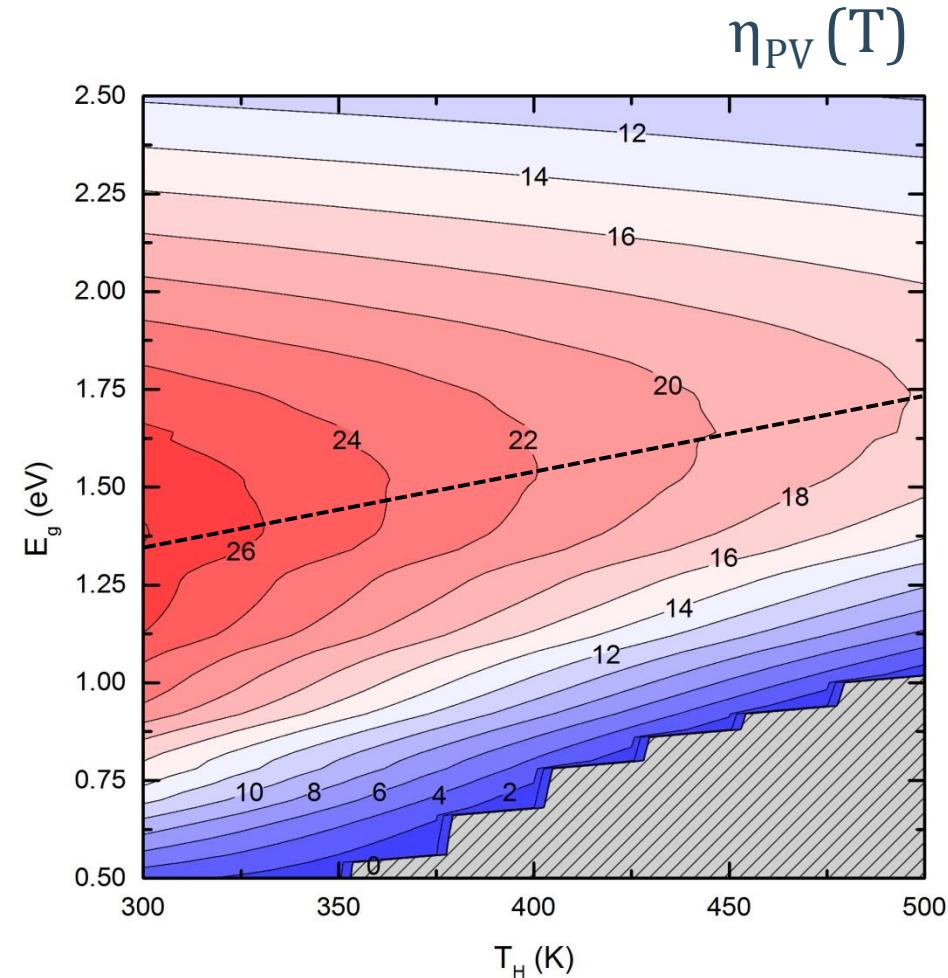


A. Virtuani, et al.; Proc. 25<sup>th</sup> UE-PVSEC, Sept. 2010, Valencia, Spain

M. Green, et al.; Prog. Photovolt. Res. Appl., 22, 1–9 (2014)

P. Singh, et al.; Sol. En. Mat. & Sol. Cells, 101 (2012) 36-45

# Accounting also for recombination



# Sub-Gap Absorber

## Case 1 (non SGA)

$$L_{2b}(E_g)\Phi_{\text{sun}} = \frac{1}{R_T}(T_{\text{cell}} - T_a)$$

$$P_{\text{TEG}}^{\text{out}} = \eta_{\text{TEG}} L_{2b}(E_g) \Phi_{\text{sun}}$$

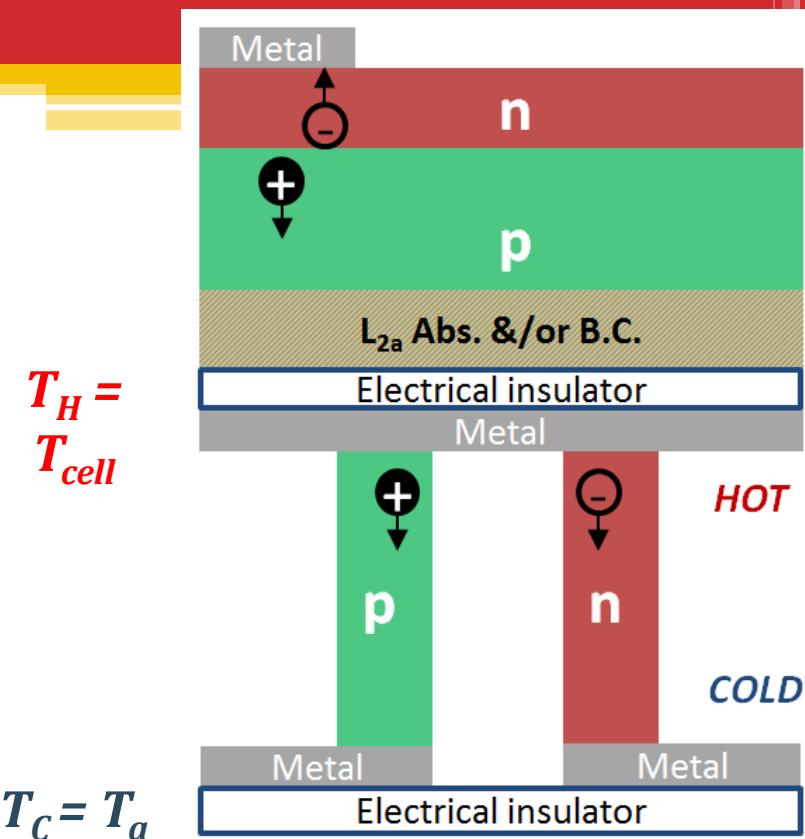
## Case 2 (SGA)

$$(L_{2a}(E_g) + L_{2b}(E_g))\Phi_{\text{sun}} = \frac{1}{R_T}(T_{\text{cell}} - T_a)$$

$$P_{\text{TEG}}^{\text{out}} = \eta_{\text{TEG}} [L_{2a}(E_g) + L_{2b}(E_g)] \Phi_{\text{sun}}$$

$$\eta_{\text{TEG}}^{\text{out}} = \frac{P_{\text{TEG}}^{\text{out}}}{\Phi_{\text{sun}}} = \begin{cases} \eta_{\text{TEG}} L_{2b}(E_g) \\ \eta_{\text{TEG}} [L_{2a}(E_g) + L_{2b}(E_g)] \end{cases}$$

$$\eta_{\text{HTEPV}} = \frac{P_{\text{PV}}^{\text{out}} + P_{\text{TEG}}^{\text{out}}}{\Phi_{\text{sun}}} = \begin{cases} \eta_{\text{PV}} + \eta_{\text{TEG}} L_{2b}(E_g) \\ \eta_{\text{PV}} + \eta_{\text{TEG}} [L_{2a}(E_g) + L_{2b}(E_g)] \end{cases}$$

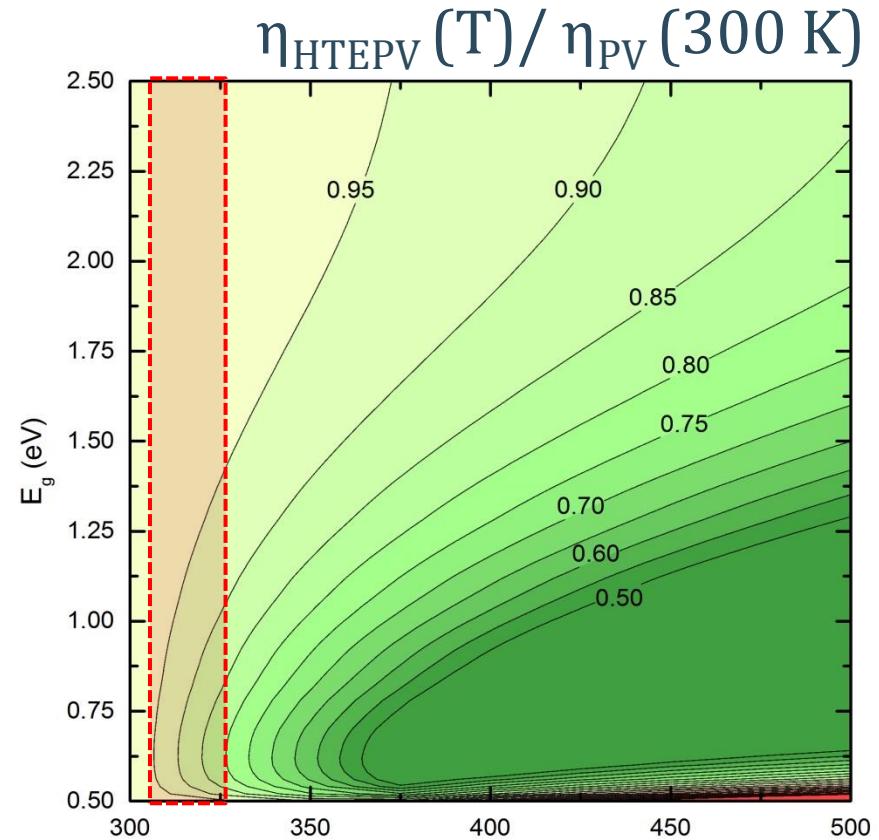
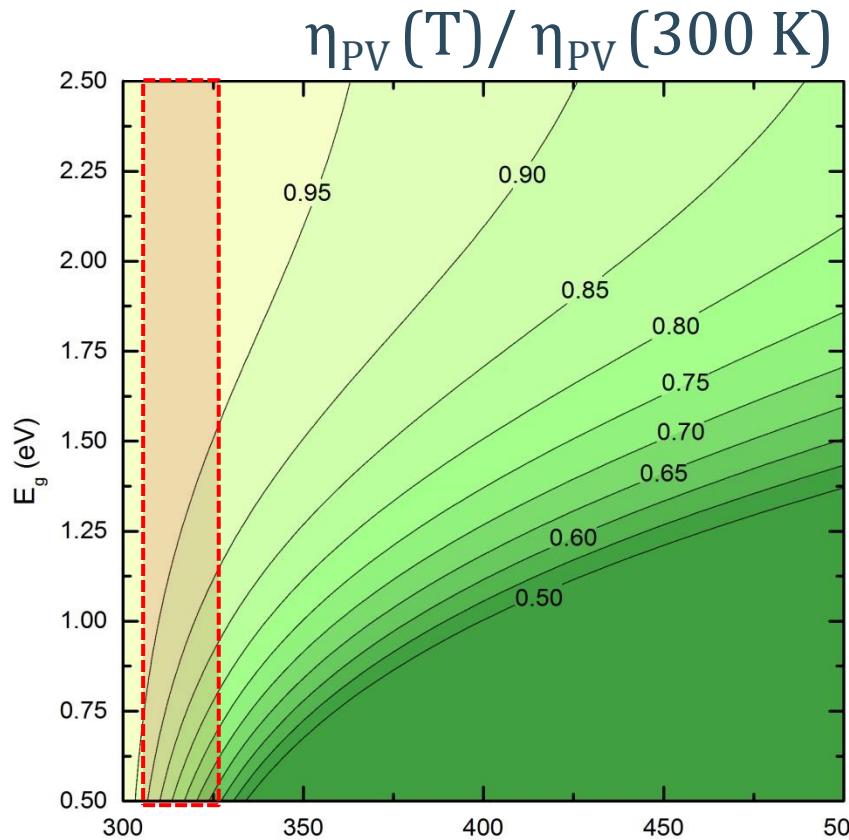


$$\eta_{\text{TEG}} = \left(1 - \frac{T_a}{T_{\text{cell}}}\right) \frac{\sqrt{1 + Z\bar{T}} - 1}{\sqrt{1 + Z\bar{T}} + T_a/T_{\text{cell}}}$$

ZT = 1

Lossless Electric Hybridization

# Non-SGA

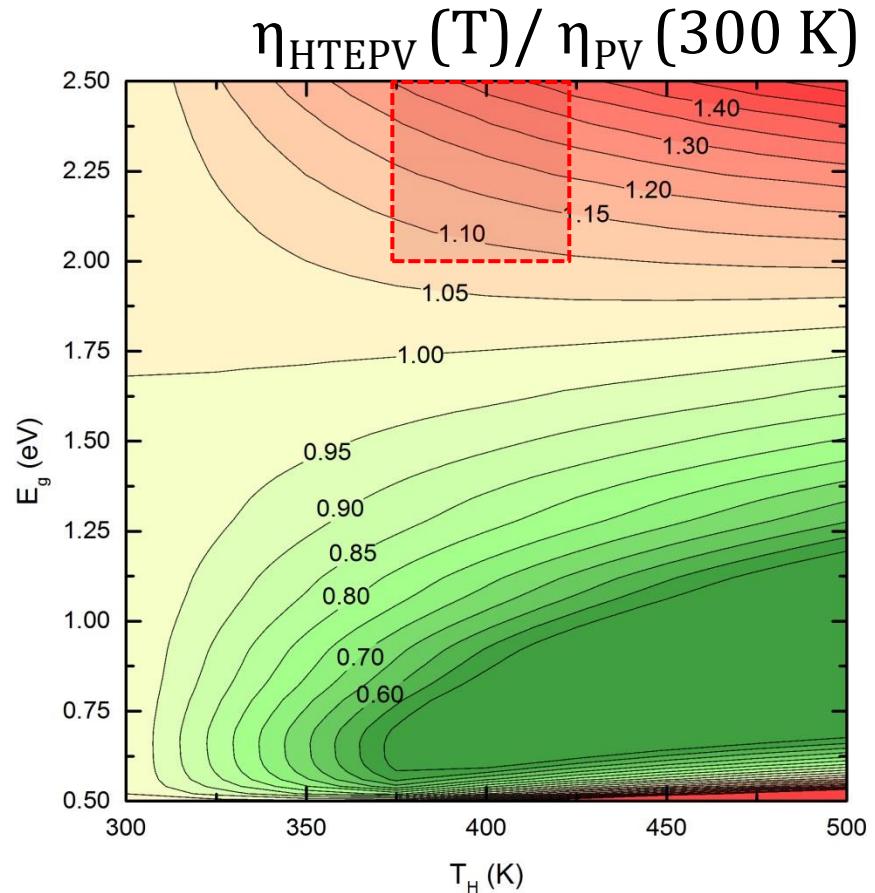
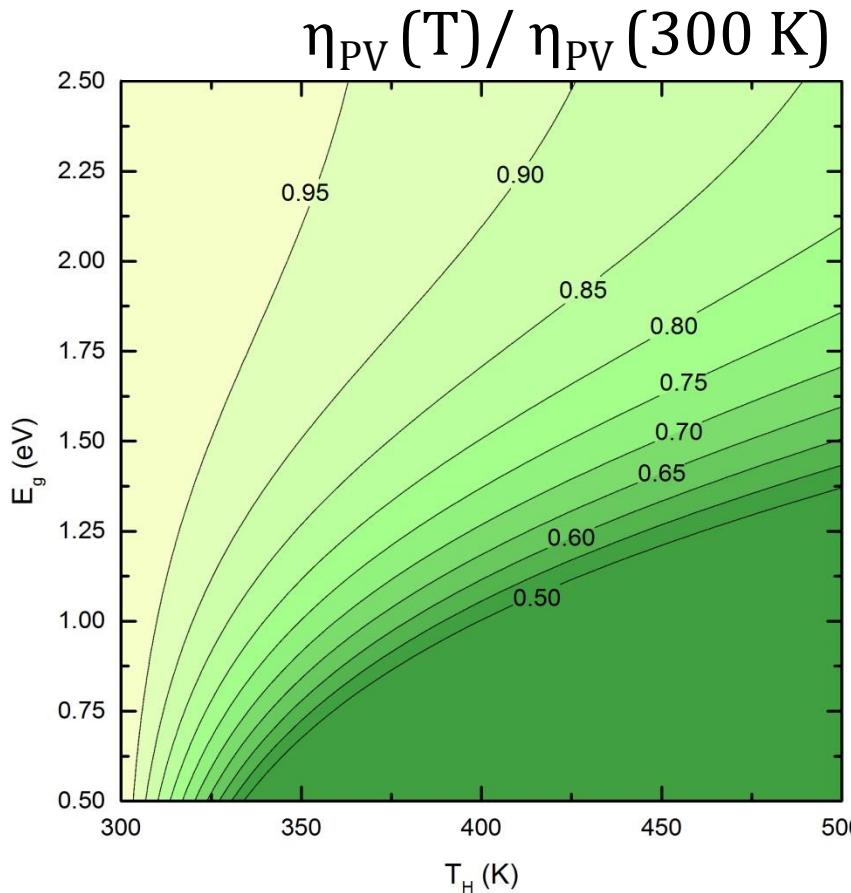


The TEG stage leads to truly minor improvements.  
Extra cost is hard to justify

E. Skoplaki; Sol. En., 83, 422 – 427 (2009)

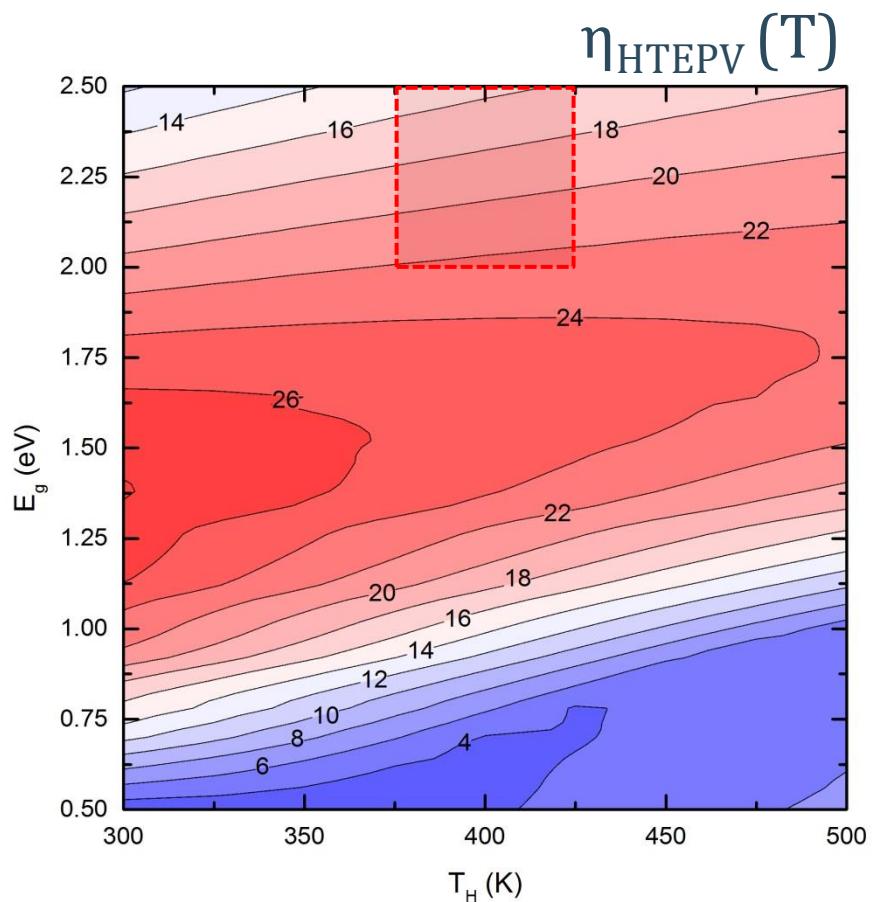
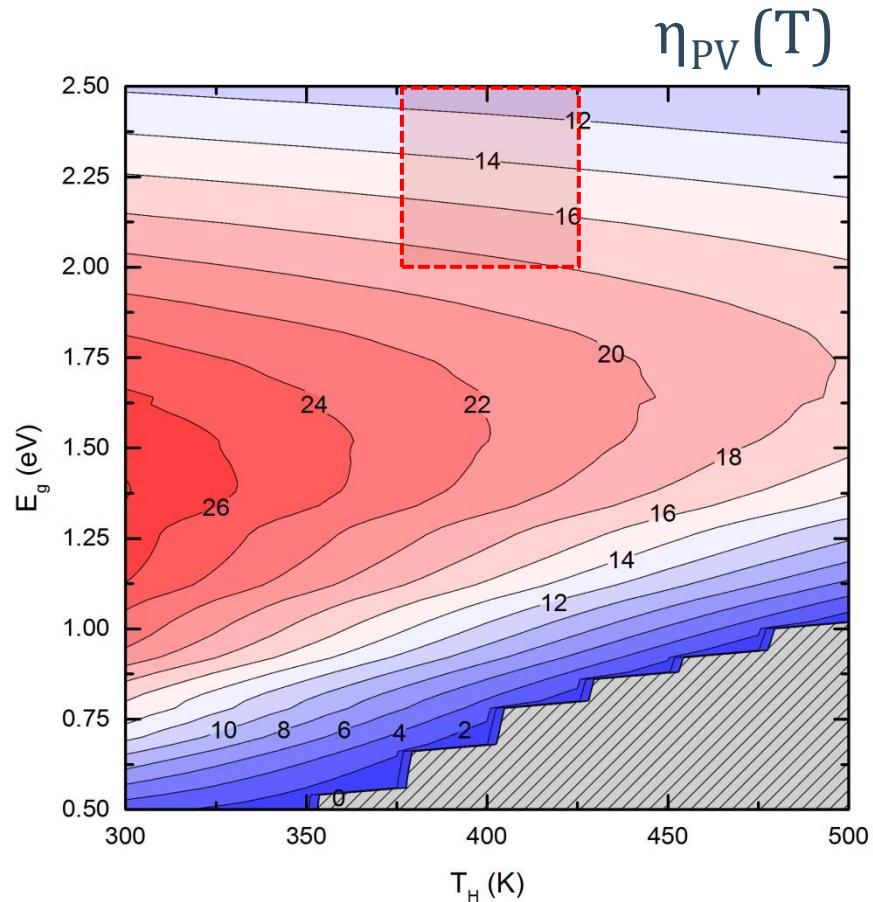
T. Nordmann and L. Clavadetscher, in Proc. 3rd WCPEC 3, 2–5 (2003)

# SGA

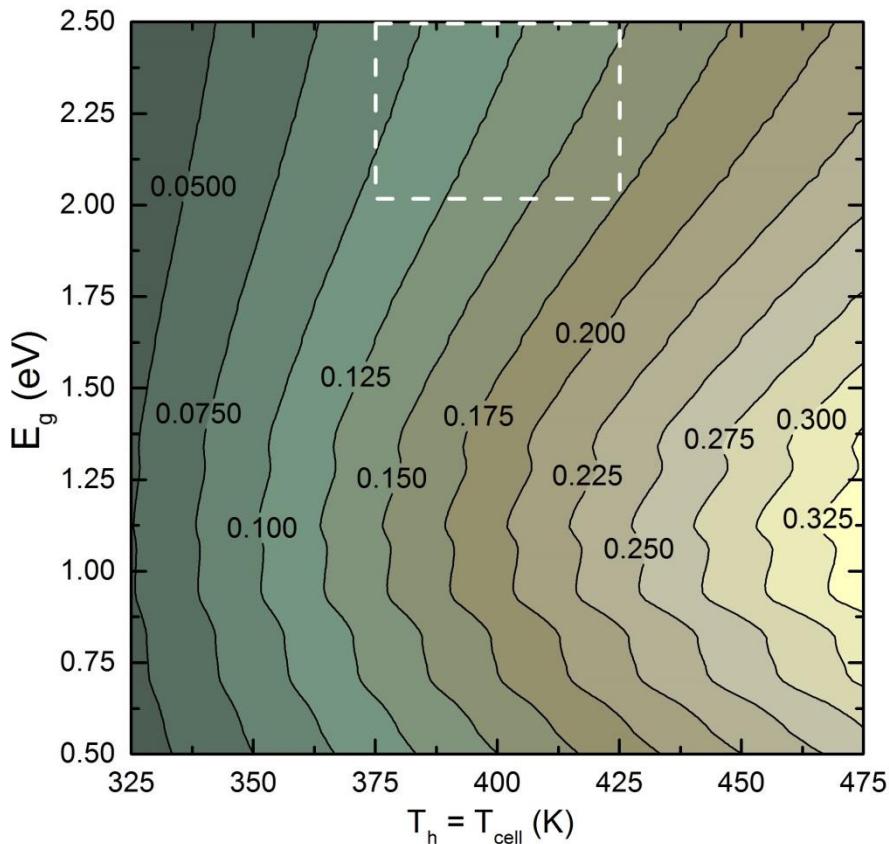


- Higher efficiencies for standard SJ solar cells with  $E_g > 1.75$  eV
- Use of wide-bandgap PV materials, normally not considered

# SGA



# Heat exchange to the ambient



$$R_T^{opt} = 0.1 - 0.175 \text{ m}^2\text{K/W}$$

## HTEPV – SGA Case

$$(L_{2a}(E_g) + L_{2b}(E_g))\Phi_{\text{sun}} = \frac{1}{R_T}(T_{\text{cell}} - T_a)$$

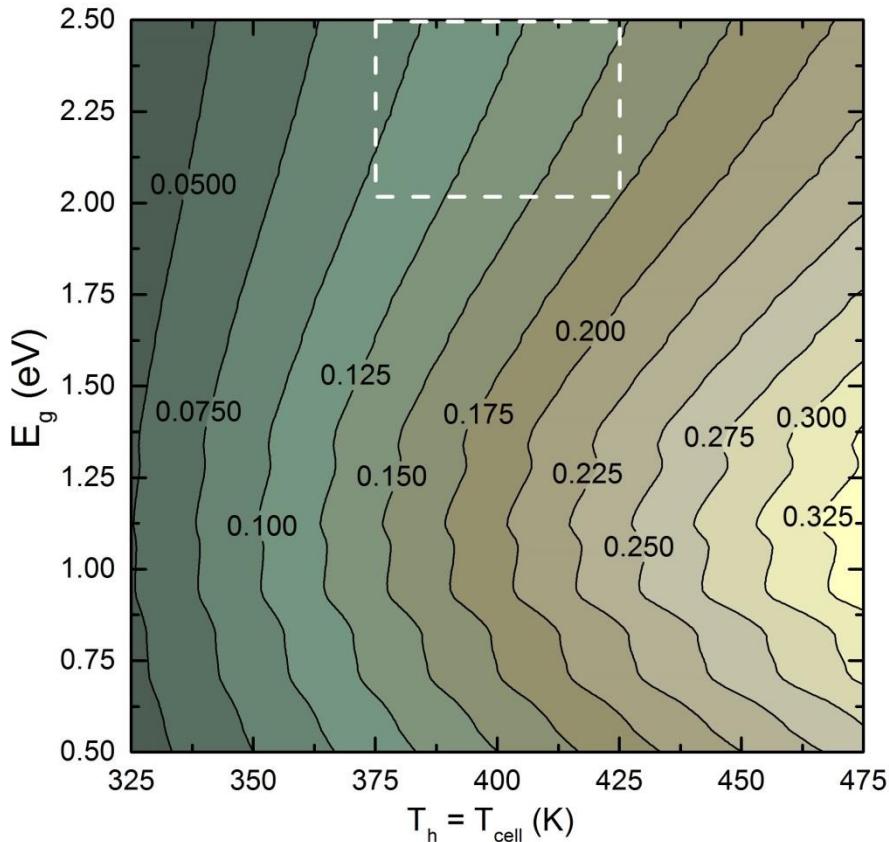


## PV only

PV array type	$R_T$ (m <sup>2</sup> K/W)
Well cooled	0.02
Free standing	0.0208
Flat on roof	0.026
Not so well cooled	0.0342
Transparent PV	0.0455
Façade integrated	0.0538
On sloped roof	0.0563

x 50

# Heat exchange to the ambient



$$R_T^{opt} = 0.1 - 0.175 \text{ m}^2\text{K/W}$$

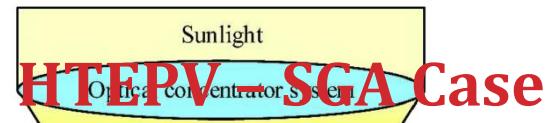
## HTEPV – SSA Case

$$(L_{2a}(E_g) + L_{2b}(E_g))\Phi_{\text{sun}} = \frac{1}{R_T}(T_{\text{cell}} - T_a)$$

**PV only**

PV array type	$R_T$ (m <sup>2</sup> K/W)
Well cooled	0.02
Free standing	0.0208
Flat on roof	0.026
Not so well cooled	0.0342
Transparent PV	0.0455
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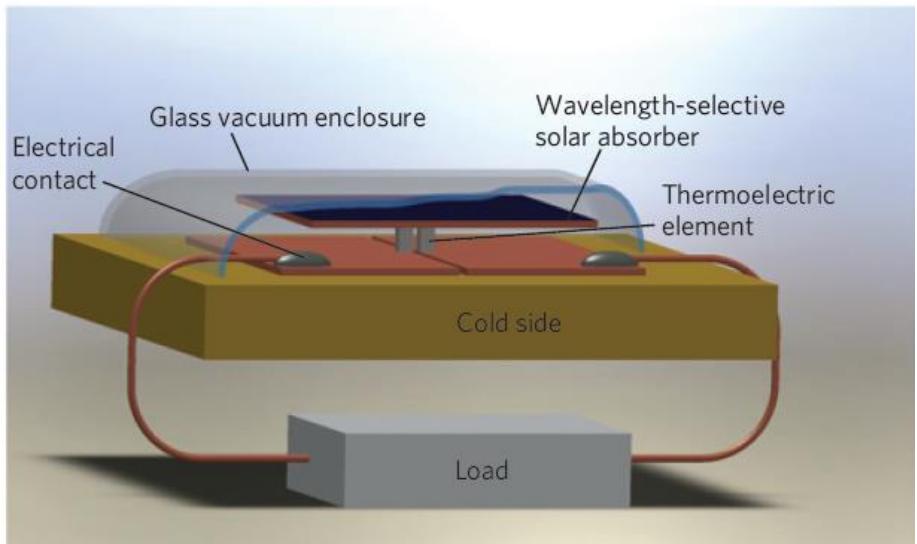
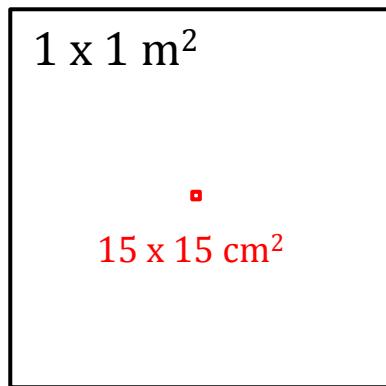
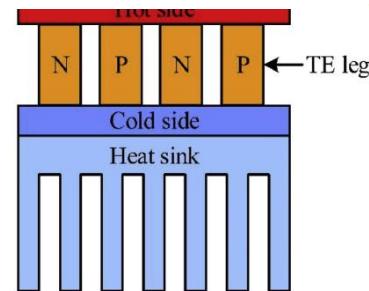
# Heat exchange to the ambient



$$(L_{2a}(E_g) + L_{2b}(E_g))\Phi_{\text{sun}} = \frac{1}{R_T}(T_{\text{cell}} - T_a)$$

Optical concentration enables standard  
TEGs

Thermal concentration >> reduced TEGs



J. Zhang et al.; Energy 78, 895 – 903 (2014)

D. Kraemer et al.; Nat. Mater. 10, 422 – 427 (2011)

# Summary

- STEGs are effective test benches to implement thermal concentration strategies
- STEGs will compete with PVs only for  $ZT > 2$
- SGA-HTEPV proves hybridization advantages:
  - Higher efficiencies for PVs with  $E_g > 1.75$  eV
  - New possibilities for wide-bandgap PV materials
  - Need for optical or thermal concentration due to thermal matching

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